

MEMS Variable Inductor for Multi-band RF CMOS Circuits

Hirota Sugawara, Yoshiaki Yoshihara, Hiroyuki Ito, Kenichi Okada, and Kazuya Masu

Precision and Intelligence Laboratory, Tokyo Institute of Technology, Japan

1. Background

On-chip inductors

The demand has been increasing for RF Si CMOS circuits.

Purpose

To realize a variable inductor on Si CMOS chip

The wireless communication system has several frequency bands which are required to cover several frequency bands.

Multi-band solutions are required to cover several frequency bands.

Variable RF Inductor

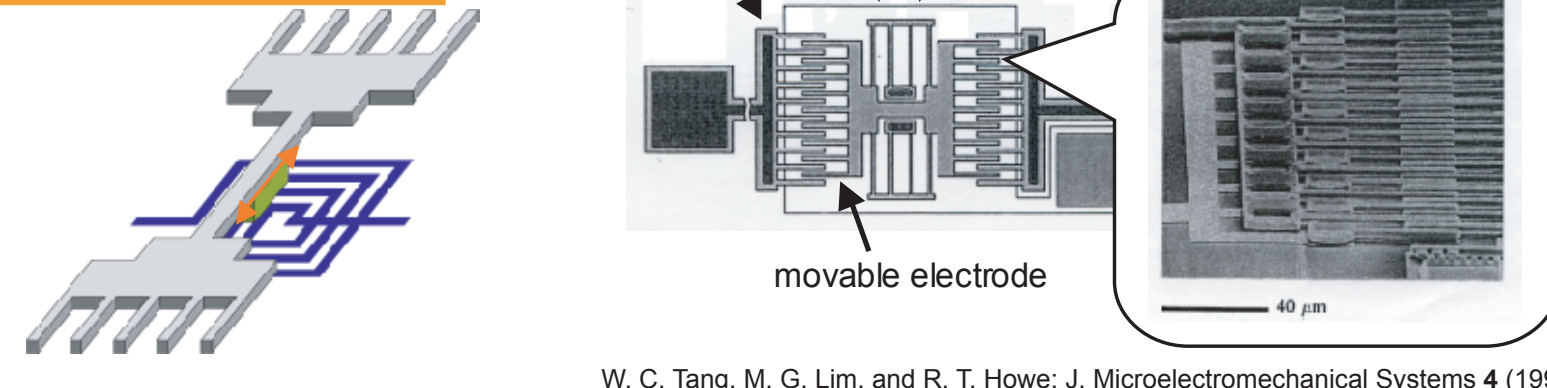
- Wide-range oscillation of VCO
- Wide-tunable impedance matching

MEMS Actuator

The actuators are driven by electrostatic force. By generating DC bias between the stationary electrode and the movable electrode.

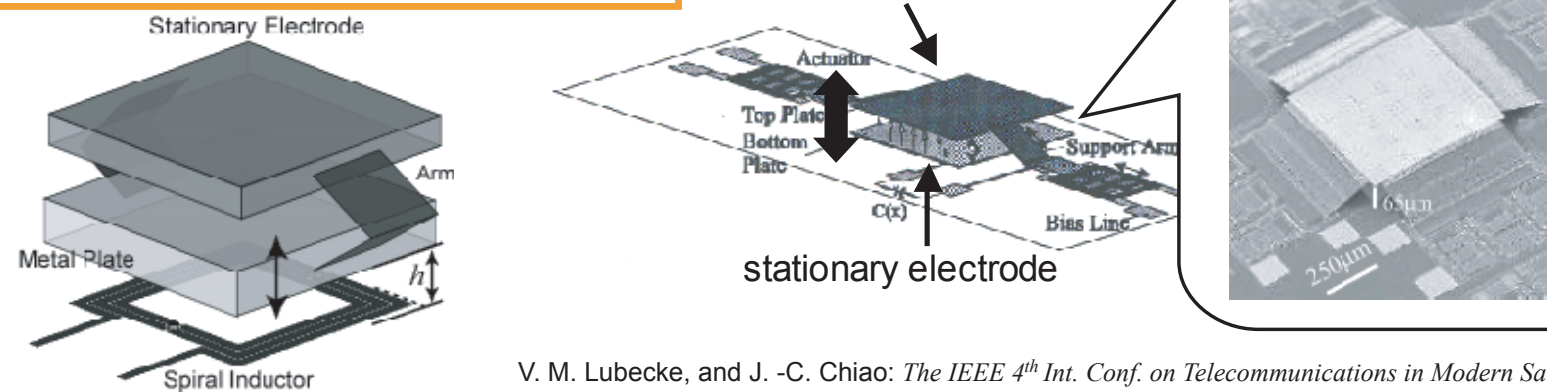
MEMS actuator is used for moving the metal plate above the spiral inductor

Comb actuator



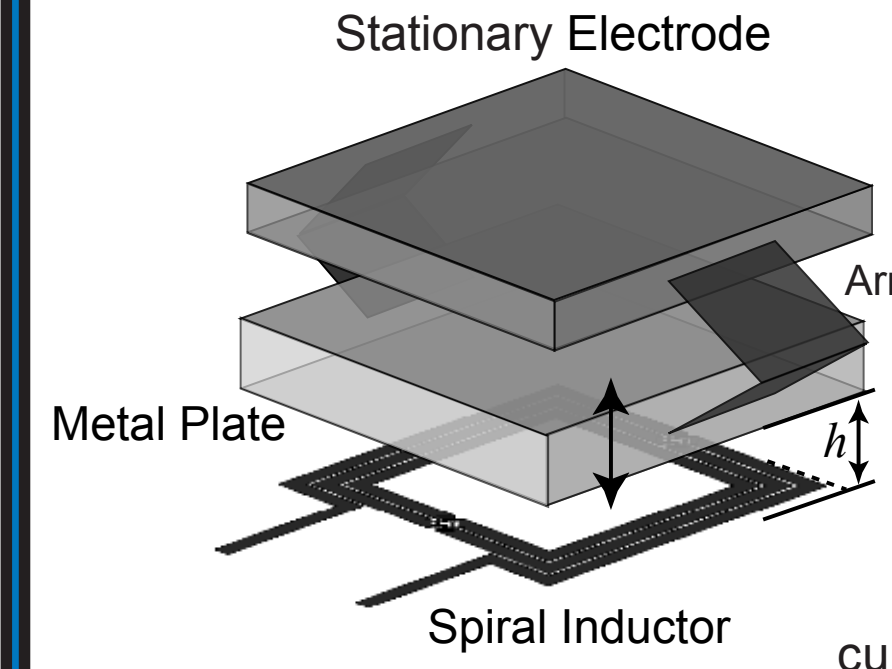
W. C. Tang, M. G. Lim, and R. T. Howe: J. Microelectromechanical Systems 4 (1992) 170.

Parallel-plate actuator



V. M. Lubbecke, and J.-C. Chiao: The IEEE 4th Int. Conf. on Telecommunications in Modern Satellite, Cable and Broadcasting Services, 1999 p. 1.

Parallel-plate Actuator



The metal plate is moved by DC bias between the stationary electrode and the movable electrode

Lower Power Consumption

current does not flow between the electrodes

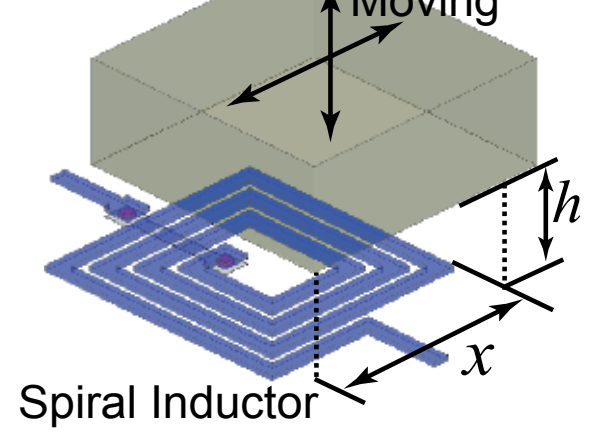
The variable inductor is an indispensable device for high-frequency and multi-band circuits.

MEMS actuator requires high manufacturing cost, and the reliability is not so high at the present time.

2. Principle of Variable Inductor

Variable Inductor

consists of a planar-type spiral inductor and a metal plate.

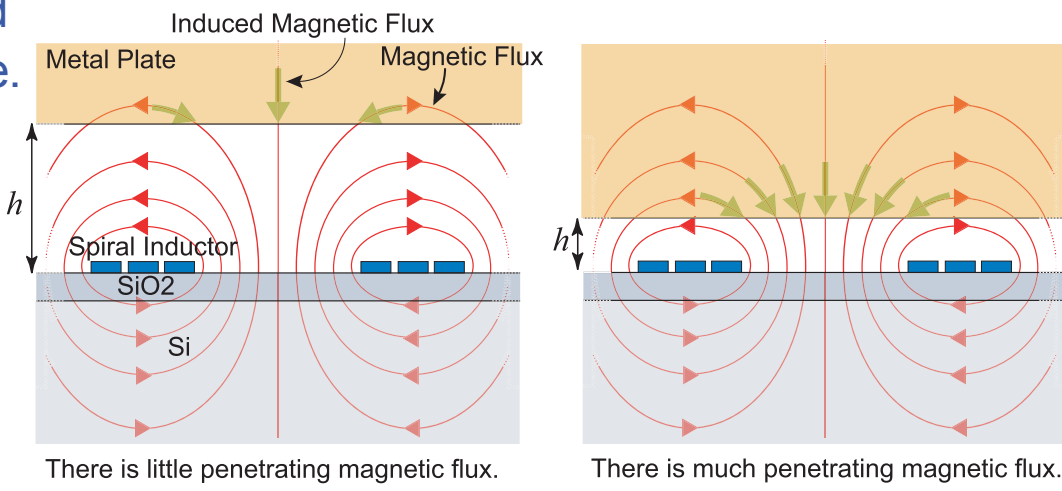


The metal plate shields the magnetic flux which penetrate the inductor.

The inductance continuously varies depending on the position of the metal plate.

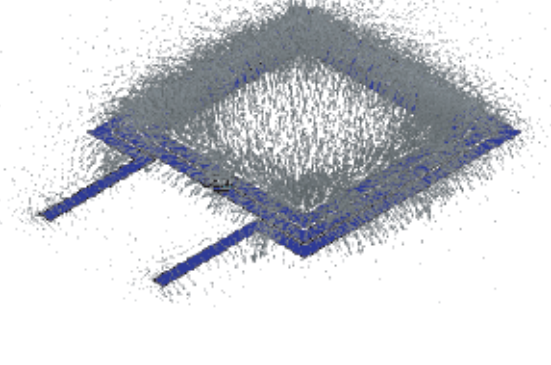
The inductance value can be also varied by changing the height of the metal plate.

- Small h
- Variable range of inductance increases.
 - Parasitic Capacitance increases.

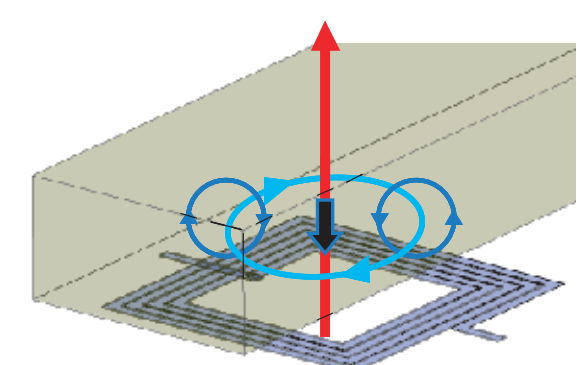
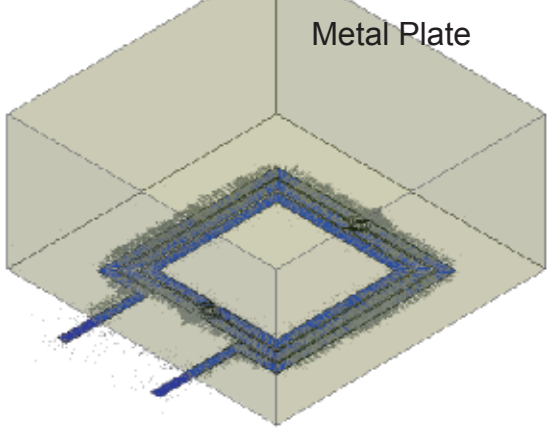


Shielding Magnetic Mechanism

[without inserting]



[with inserting]



The magnetic flux penetrates the metal plate.

Eddy current flows in the metal plate.

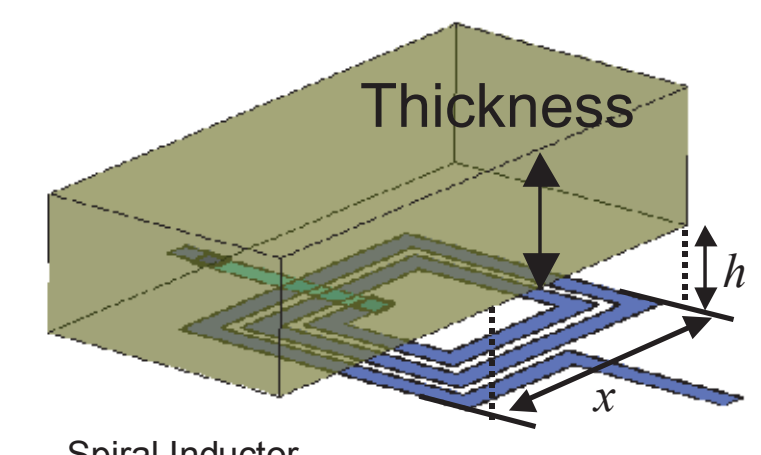
Induced a counteractive magnetic field according to Lenz's Law.

The metal plate shields the magnetic flux.

Change of the magnetic flux

Inductance change

Metal Plate



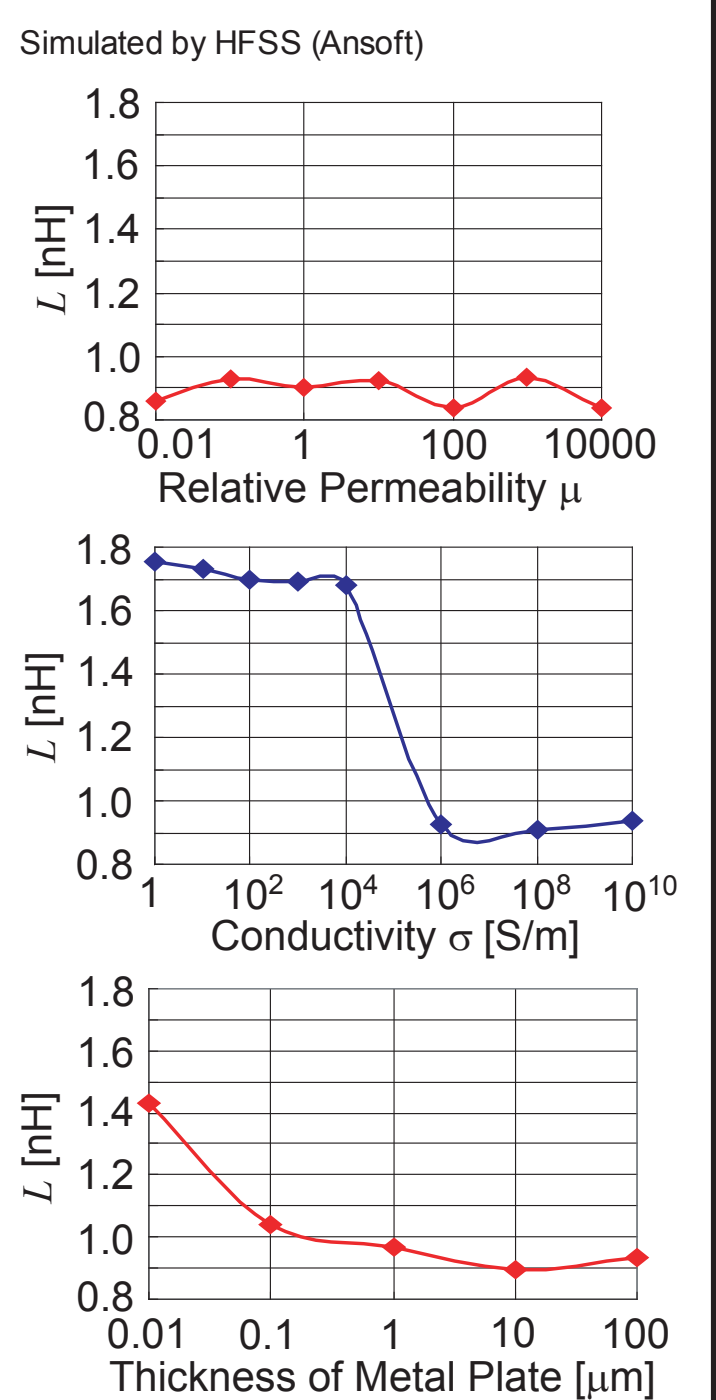
Spiral Inductor
Turns : 2.5
Line width W : 20 μm
Line space S : 10 μm
Outer dimension D : 250 μm
L=1.8 nH

$$\text{Skin Depth} = \sqrt{\frac{2}{\omega\sigma\mu}}$$

Skin Depth = 2 μm @ 1GHz

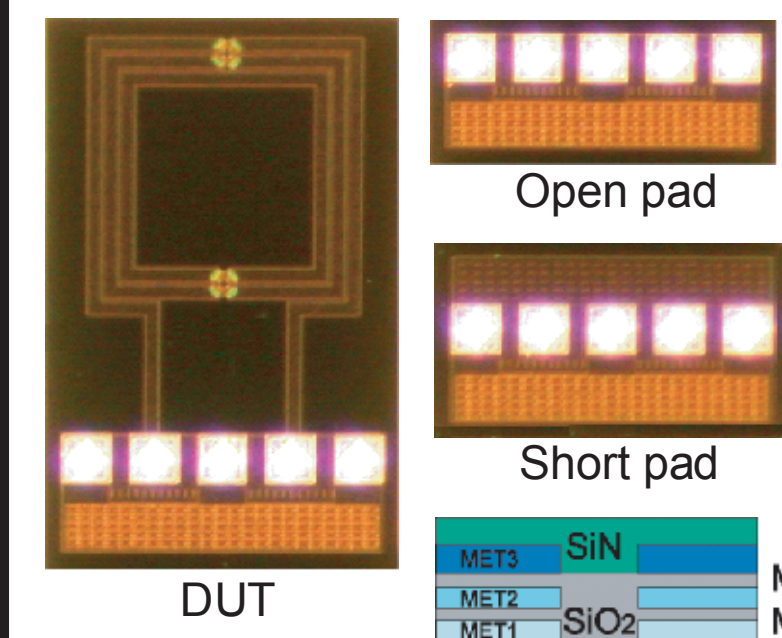
Metal Thickness of over Skin Depth

Magnetic flux can be shielded by the metal plate



3. Measurement Results

Measurement Method



$$L = \frac{1}{\omega} \text{Im}(Z_d)$$

$$Q = \frac{\text{Im}(Z_d)}{\text{Re}(Z_d)}$$

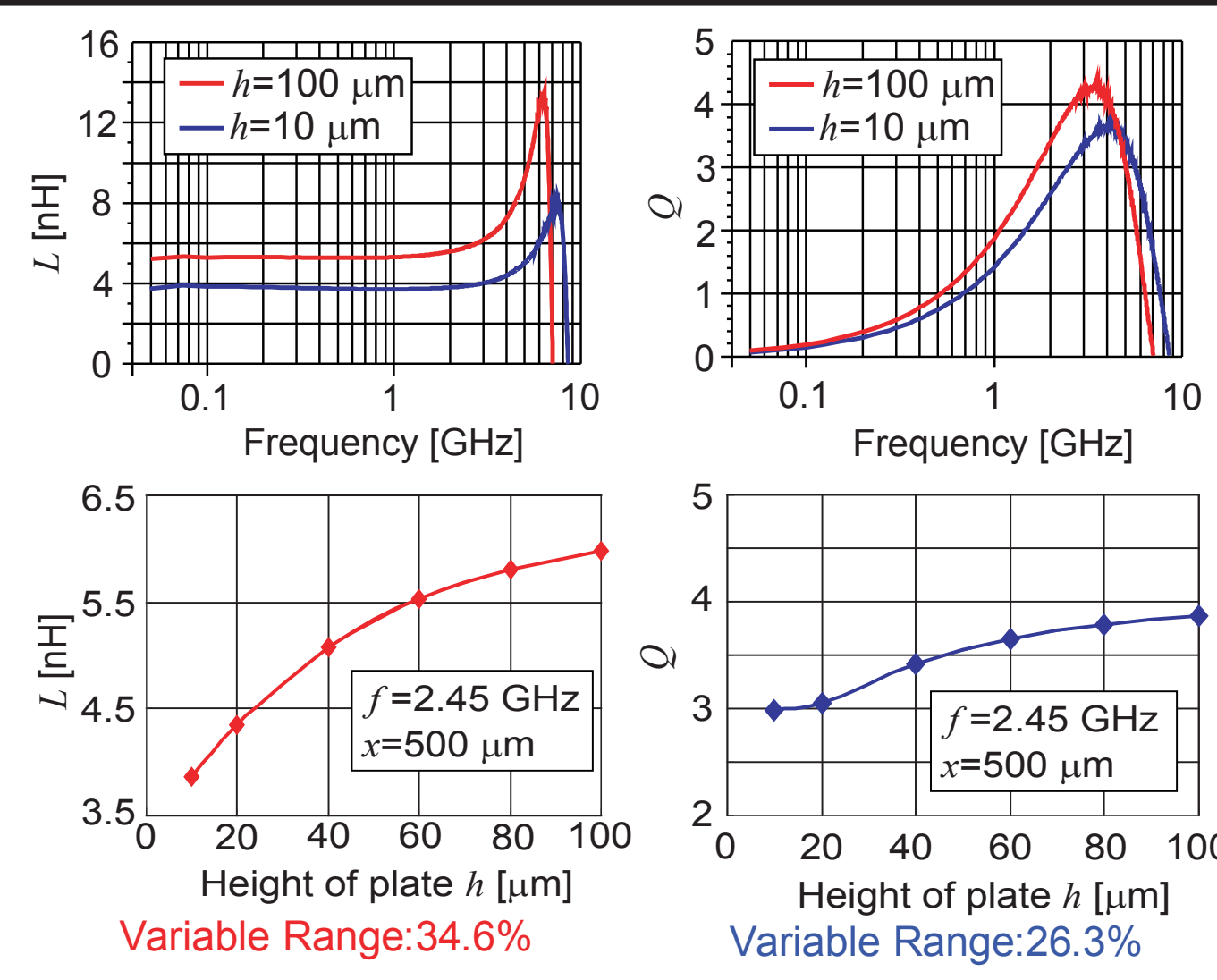
$$Z_d = Y_{11}^{\text{ind}} + Y_{12}^{\text{ind}} + 2Y_{12}^{\text{ind}}$$

$$Z_d = \frac{Y_{11}^{\text{ind}} Y_{22}^{\text{ind}} - (Y_{12}^{\text{ind}})^2}{Y_{11}^{\text{meas}} - Y_{11}^{\text{open}} - Y_{22}^{\text{meas}} + Y_{22}^{\text{open}}}$$

De-embedding

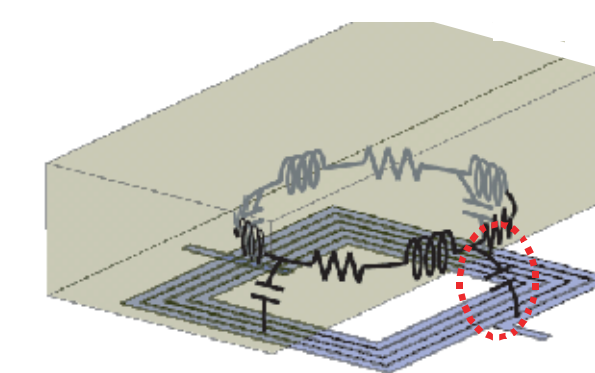
Open and short pad are used

$$Y^{\text{ind}} = \frac{1}{Y^{\text{meas}} - Y^{\text{open}} - Y^{\text{short}} + Y^{\text{open}}}$$



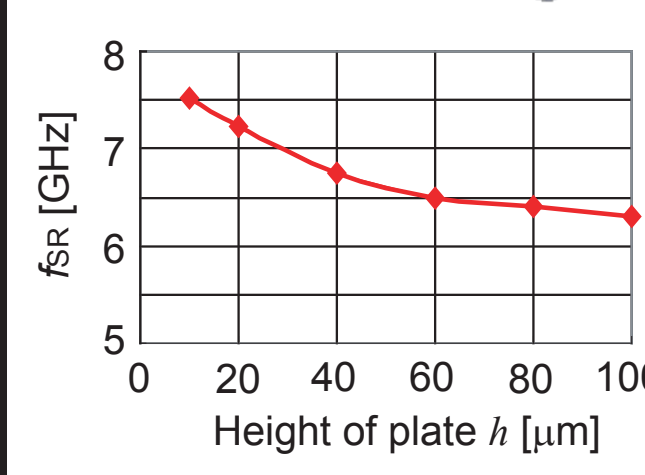
The variation Q is smaller than that of L

Effect of Parasitic Capacitance



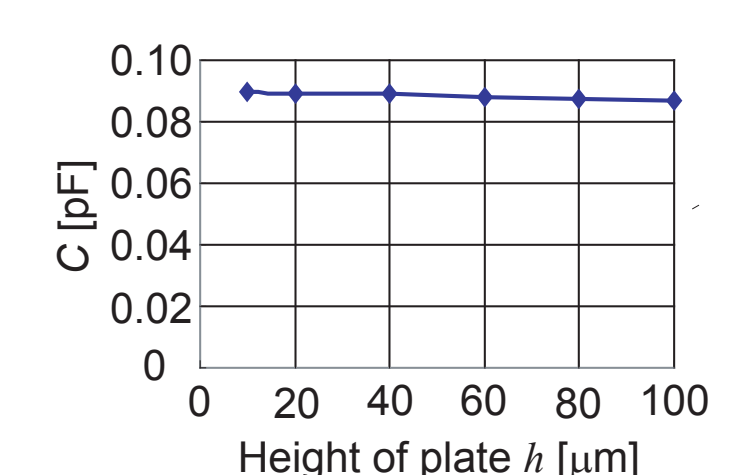
The parasitic capacitance is induced between the spiral inductor and the metal plate

⇒ Degrade the inductor characteristics



h decreases ⇒ f_{SR} decreases

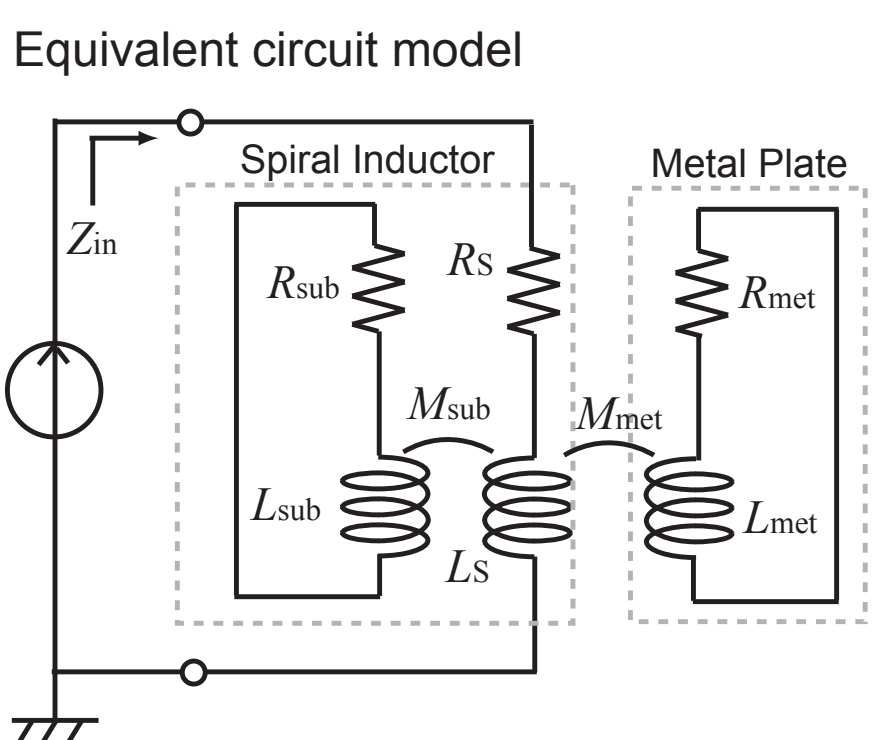
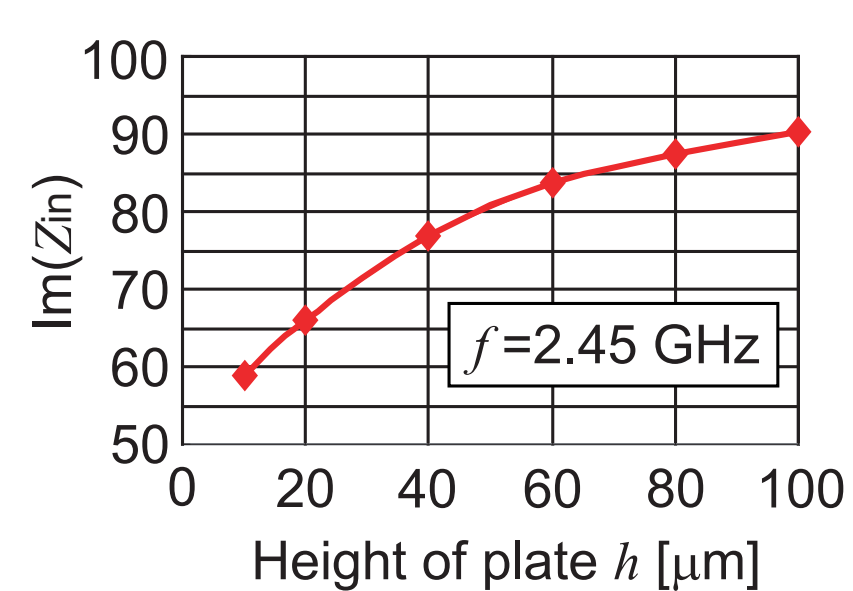
Effect of parasitic capacitance is not dominant



Parasitic capacitance is not increased so much by metal plate

$$f_{SR} = \frac{1}{2\pi\sqrt{LC}}$$

Input Impedance



$$Z_{in} = R_s + j\omega L_s + \frac{(\omega M_{met})^2}{R_{met} + j\omega L_{met}} + \frac{(\omega M_{sub})^2}{R_{sub} + j\omega L_{sub}}$$

$$= R_s + \frac{(\omega M_{met})^2 R_{met}}{R_{met}^2 + (\omega L_{met})^2} + \frac{(\omega M_{sub})^2 R_{sub}}{R_{sub}^2 + (\omega L_{sub})^2}$$

$$+ j \left(L_s - \frac{(\omega M_{met})^2 \omega L_{met}}{R_{met}^2 + (\omega L_{met})^2} - \frac{(\omega M_{sub})^2 \omega L_{sub}}{R_{sub}^2 + (\omega L_{sub})^2} \right)$$

h decreases ⇒ M_{met} increases ⇒ $\text{Im}(Z_{in})$ decreases
 h decreases ⇒ M_{sub} decreases ⇒ $\text{Re}(Z_{in})$ decreases

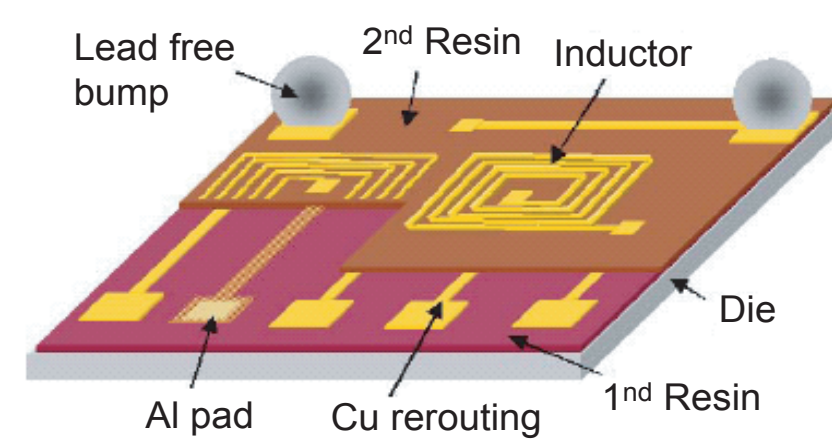
$$Q = \frac{\text{Im}(Z_{in})}{\text{Re}(Z_{in})} \Rightarrow \text{Variation of } Q \text{ is small}$$

Appendix. Redistributed Layers

WL-CSP wafer-level chip-scale packages

WL-CSP

The CMOS chip's pads are connected to the board's pads through lead free bumps and redistributed layers.



K. Itoi, M. Sato, H. Abe, H. Sugawara, H. Ito, K. Okada, K. Masu, and T. Ito: IEEE MTT-S Int. Microwave Symp. Digest, Fort Worth, 2004 p. 197.

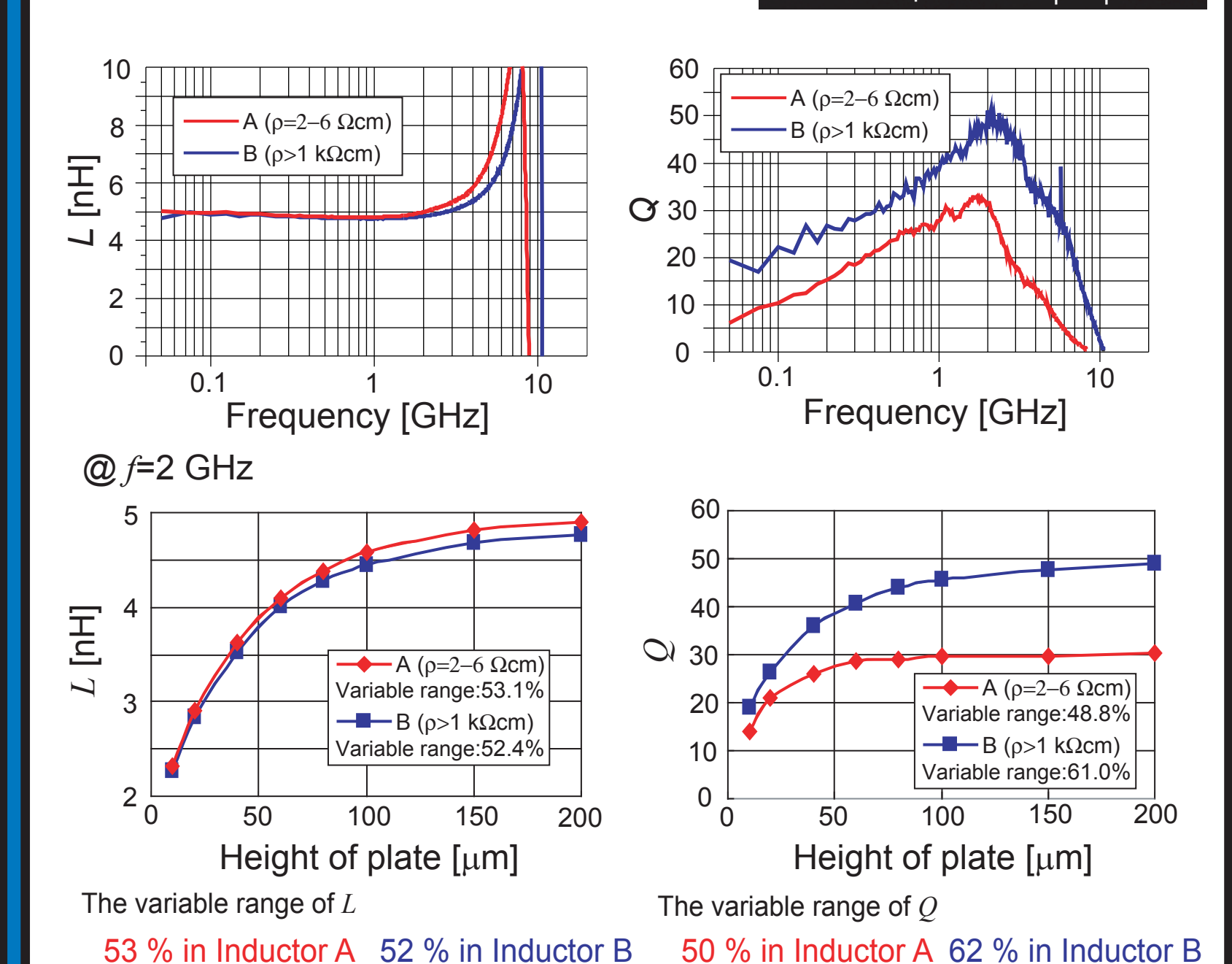
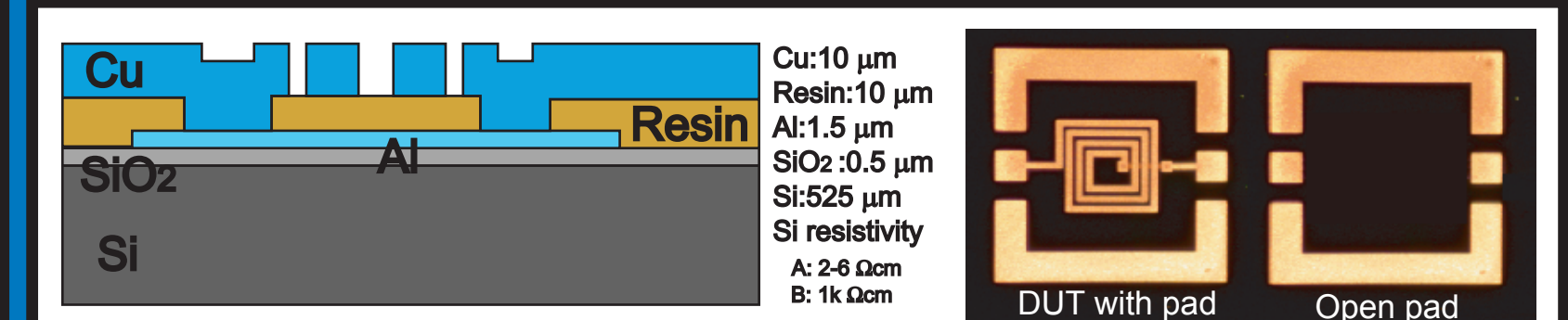
Inductance is implemented using redistributed layer

WL-CSP Advantages

- Thick Cu conductor
- Resin layer between the conductor and Si substrate

Reduction in substrate loss

⇒ High-Q



The variable range of L
 53% in Inductor A 52% in Inductor B
 The variable range of Q
 50% in Inductor A 62% in Inductor B